## Status of optics modeling at the MLS and at BESSY II

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$\square$ LOCO
$\square$ Status of optics' studies
$\square$ Reducing the coupling
$\square$ Symmetrizing the optics
$\square$ Results

## Linear Optics from Closed Orbits (LOCO)



## Introduction

$\square$ LOCO: Linear Optics from Closed Orbits.
$\square$ Simulation programs (e. g. MAD) can compute response matrices for a given lattice.
$\square$ LOCO uses the opposite approach: Attempt to reconstruct the linear optics from measured response matrices.
$\square$ A successful LOCO analysis helps improving the understanding of the status of the storage ring.

## Objective

Determining the
$\square$ quadrupole gradients.
$\square$ BPM gains.
$\square$ calibration factors of the steerer magnets.
$\square$ conversion factors of the skew quadrupole gradients.
$\square$ BPM coupling.
$\square$ quadrupole roll.
$\square$ focusing properties of IDs.

## Plot of a Response Matrix


$\square$ Kick the beam horizontally/vertically and record the response at the BPMs.

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## Response matrix of the model

Response matrix $M_{i j}$ :
change in orbit at BPM $i$ depending on the strength $\theta_{j}$ of the corrector magnet $j$

$$
\left[\begin{array}{l}
x \\
y
\end{array}\right]=M\left[\begin{array}{l}
\theta_{x} \\
\theta_{y}
\end{array}\right]
$$

$\square$ Vertical response matrix:

$$
M_{i j}=\frac{\sqrt{\beta_{i} \beta_{j}}}{2 \sin \pi \nu} \cos \left(\left|\phi_{i}-\phi_{j}\right|-\pi \nu\right)
$$

$\square$ Horizontal response matrix:

$$
M_{i j}=\frac{\sqrt{\beta_{i} \beta_{j}}}{2 \sin \pi \nu} \cos \left(\left|\phi_{i}-\phi_{j}\right|-\pi \nu\right)-\frac{\theta_{j} \eta_{j}}{\alpha_{c} L_{0}} \eta_{i}
$$

Dispersive term in the horizontal plane:

- $\beta_{i}$ beta function
- $\phi_{i}$ phase advance
- $\eta_{i}$ dispersion
- $\nu$ tune
- $\alpha_{c}$ momentum compaction factor
- $L_{0}$ length of the ring

The length of the orbit is determined by the RF frequency:
$\rightarrow$ The change in path length caused by the kick has to be offset by
a change in energy keeping the revolution time constant.

## Method

$\square$ The parameters in the model are varied.
$\square$ Goal: Minimizing the difference between measured and simulated response matrix.
Figure of merit

$$
\chi^{2}=\sum_{i=1}^{n} \sum_{j=1}^{m} \frac{\left(M_{i j}^{\text {meas }}-M_{i j}^{\text {model }}\right)^{2}}{\sigma_{i}^{2}}=\sum_{k=i, j}^{N} E_{k}^{2}
$$

The error vector is minimized by iteration. (SVD, Gauß-Newton method)

$$
\begin{aligned}
E_{k}^{\text {new }} & =E_{k}+\frac{\partial E_{k}}{\partial K_{l}} \Delta K_{l} \\
-E_{k} & =\frac{\partial E_{k}}{\partial K_{l}} \Delta K_{l}
\end{aligned}
$$

- $\sigma_{i}$ : noise level of the BPMs
- $E_{k}$ : error vector
$\square K_{l}$ : fit parameter; gradient, gain, etc.
- $\sigma($ model - meas $):=$ standard deviation $\left(M_{i j}^{\text {model }}-M_{i j}^{\text {meas }}\right)$

The response matrix is not a linear function of the quadrupole gradients. Fit needs to be iterated until convergence occurs.

## BESSY II

$\square$ Double bend
 achromat lattice
$\square$ eight super cells
$\square$ Circumference $L=240 \mathrm{~m}$.
$\square$ Nominal Energy $E=1.72 \mathrm{GeV}$.
$\square$ Emittance
$\epsilon_{x}=6 \mathrm{~nm} \mathrm{rad}$.
$\square$ Emittance
$\epsilon_{x}=4 \mathrm{~nm} \mathrm{rad}$
including super
conducting devices.

## Fit parameters for BESSY II

$\square 108$ horizontal BPM gains
$\square 108$ vertical BPM gains
$\square 80$ horizontal corrector magnet gains
$\square 64$ vertical corrector magnet gains
$\square 44$ circuits (quadrupole gradients)
in total: $M=404$ fit parameters
Measurement data:
$\square 108 \times 80+108 \times 64$ data points included in the response matrix
$\square 108$ dispersion measurements
in total: $N=15660$ data points number of degrees of freedom $N-M=15256$

$$
\chi^{2}=N-M \pm \sigma, \quad \sigma=\sqrt{2(N-M)}
$$

Predictor for the statistical error if $N-M$ is asymptotically large.

## Best fit

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$\square$ The predictor for the precision of the fit, $\sigma$ (model measurement), reaches (almost) the noise level of the BPMs
$\square$ Only sextupole family S 1 is excited, $I_{S 1}=40 \mathrm{~A}$

- $\sigma$ (model measurement) $=$ $0.69 \mu \mathrm{~m}$
- Average of the BPM $\sigma$ s:
horizontal: $0.59 \mu \mathrm{~m}$, vertical: $0.54 \mu \mathrm{~m}$


## Analysis for different machine settings

- WLS: Wave Length Shifter.
- FFF: Fast Feed Forward (IDs).

| Setting | $\frac{\chi^{2}}{D O F}$ | $\sigma$ (model - meas.) |
| :---: | :---: | :---: |
| only S1 minimal | 1.525 | $0.687 \mu \mathrm{~m}$ |
| + skews | 1.479 | $0.672 \mu \mathrm{~m}$ |
| user optics | 3.975 | $0.746 \mu \mathrm{~m}$ |
| + skews | 9.138 | $1.046 \mu \mathrm{~m}$ |
| user optics w/ WLS/FFF | 4.350 | $0.805 \mu \mathrm{~m}$ |
| + skews | 8.019 | $1.002 \mu \mathrm{~m}$ |

$\square$ CQS: Skew Quadrupoles.

- User optics: All sextupoles including harmonic ones are at standard settings.
- Average of the BPM $\sigma$ s: horizontal: $0.59 \mu \mathrm{~m}$, vertical: $0.54 \mu \mathrm{~m}$


## BPM gains for different optics


$\square$ Fitting the BPM gains substantially improves the quality of the fit.

- BPM gains deviate considerably from the nominal value.
$\square\left\langle\operatorname{gain}_{x}\right\rangle \approx 0.9$ $\left\langle\right.$ gain $\left._{y}\right\rangle \approx 1$.
$\square$ BPM readings become nonlinear for large orbit excursions.


## Modeling the impact of the WLSs

$\square$ Wave length shifters (WLS) focus only vertically
$\rightarrow$ quadrupoles cannot absorb this effect.
$\square$ Modeling of WLS as thin "cylinder lenses" focusing only in the vertical plane.
$\square$ Wiggler: modeled as a sequence of dipoles.
Results - in comparison with an analysis only employing quadrupoles:
$\square \chi^{2} /$ DOF reduces by a factor of 50 .
$\square \sigma$ (model - measurement) decreases by an order of magnitude.

## Beta functions: design- and user optics




Design optics



User optics

## Checking the predictions of the model

Chromaticity:
Determining of chromaticities for the user optics without WLS and skew quadrupoles.
$\square$ measured $\xi_{x}=3.49$ and $\xi_{y}=3.95$
$\square$ from the calibrierten model:
$\xi_{x}=3.89$ und $\xi_{y}=3.86$ (thin sextupoles) or $\xi_{x}=$ 3.70 und $\xi_{y}=3.76$ (sextupole with effective length.

## Determining emittances via simulations

## Problem:

$\square$ small vertical emittances cannot be determined with the diagnostic tools available.

Approach:
$\square$ Fit a skew quadrupole gradient at the location of each sextupole.
$\square$ Get the emittances from the Ohmi-Envelope ("coupled" optical functions).

## Minimizing the coupling - procedure

Approach:
Try to minimize the vertical dispersion and the vertical emittance simultaneously employing the available skew quadrupoles.

Caveats:
$\square$ At BESSY II only three skew quadrupoles are located at dispersive sections.
$\rightarrow$ Increasing the number of skew quadrupoles in dispersive sections would help in minimizing the vertical dispersion.
$\square$ The 15 skew quadrupoles are located only in about one half of the ring.
$\rightarrow$ A more even distribution could reduce the local coupling at important locations.
$\square$ Four BPMs couple, only three buttons are functional.

## Determining the emittances: example



Principal Axis of the Beam Ellipse



Vertical Emittance


Emittance Ratio $=1.378447 \%$
$\square$ user optics including all WLSs and FFF, CQS are off.
$\square$ the horizontal emittance $\epsilon_{x}$ and the vertical $\epsilon_{y}$ vary considerably along the ring.
$\square$ WLS: Wave Length Shifter
$\square$ FFF: Fast Feed Forward (IDs)
$\square$ CQS: Skew Quads

## Coupling for given machine settings

| Optics | $\left\langle\epsilon_{y}\right\rangle$ <br> $[\mathrm{pm} \mathrm{rad}]$ | $\kappa=\frac{\epsilon_{y}}{\epsilon_{x}}$ <br> $[\%]$ | $\eta_{y \mathrm{RMS}}$ <br> $[\mathrm{mm}]$ |
| :--- | :---: | :---: | :---: |
| only S1 minimal | 14.3 | 0.22 | 5.40 |
| only S1/S2 chrom. 0 | 18.0 | 0.28 | 6.78 |
| user optics w/o WLS | 74.6 | 1.13 | 7.66 |
| user optics w/ WLS/FFF | 93.3 | 1.38 | 9.91 |
| user optics w/WLS/FFF <br> u. CQS | 99.8 | 1.48 | 7.90 |

$\square$ The coupling is mainly induced by the orbit excursions in the harmonic sextupoles and not by the settings of the skew quadrupoles.

- Average vertical emittance $\left\langle\epsilon_{y}\right\rangle$
$\square$ Coupling $\kappa=\epsilon_{y} / \epsilon_{x}$
- Vertical Dispersion (RMS) $\eta_{y \text { RMS }}$
- WLS: Wave Length Shifter
- FFF: Fast Feed Forward (IDs)
- CQS: Skew Quads


## Decoupling - iterative process



## Decoupling - comparing the results with measurements

Criterion: reduction of the (Touschek) life time at large beam current ( $I \approx 300 \mathrm{~mA}$ )

| mode | life time |
| :---: | :---: |
| 3rd iteration | 6.9 h |
| 2nd iteration | 7.0 h |
| 1st iteration | 7.7 h |
| CQS off | 11.9 h |
| CQS standard | 10.7 h |

- All Sextupoles and the WLS are at their standard settings. (user optics)
$\square$ The ellipse at the beam profile monitor assumes normal orientation.
$\rightarrow$ The life time can be reduced by $40 \%$.


## Symmetrizing the optics

## Objective:

$\square$ Restoring the dynamic aperture.
$\square$ Dialing in the reference optics in a reproducible fashion.

Approach:
$\square$ Determine the normalized quadrupole gradients per circuit.
$\square$ Changing the quadrupole settings according to

$$
\frac{\Delta I_{n}}{I_{n}}=-\frac{K_{\mathrm{fit}, n}-K_{\mathrm{ref}, n}}{K_{\mathrm{ref}, n}}
$$

employing offset channels at the quadrupole power supplies.

Caveats:
$\square$ Quadrupoles at BESSY II cannot be powered individually.
Q Q1D/T and Q2D/T: 16 quadrupole each are ganged together.
$\square$ Q3D/T, Q4D/T and Q5T can be powered in pairs.

## Restoring the beta functions

$\square$ User optics without WLSs
$\square \beta_{\text {iref }}: \beta$ function of the reference.
$\square \beta_{i \mathrm{sym}}: \beta$ function of the symmetrized optics
$\square \beta_{i 0}: \beta$-function before symmetrizing.

| Iteration | Beta beat RMS |  |
| :--- | :---: | :---: |
|  | x | y |
| 0. | $6.95 \%$ | $4.39 \%$ |
| 1. | $0.80 \%$ | $0.97 \%$ |
| 2. | $0.44 \%$ | $0.22 \%$ |

## Restoring the phase



$\square$ user optics without WLSs
$\square \phi_{i \mathrm{ref}}$ : phase of the reference.
$\square \phi_{i s y m}$ : phase of the symmetrized optics (2nd iteration).
$\square \phi_{i 0}$ : phase before symmetrizing.

## LOCO - Low alpha optics


$\square f_{s}=1.75 \mathrm{kHz}$.
$\square \chi^{2} / D O F=$ 5.625.
$\square \sigma($ model meas.) = $1.34 \mu \mathrm{~m}$.
$\square$ BPM noise: $\left\langle\sigma_{x}\right\rangle=0.9 \mu \mathrm{~m}$, $\left\langle\sigma_{y}\right\rangle=0.4 \mu \mathrm{~m}$
$\square$ Orbit drifts during the measurement.

## The Metrology Light Source

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$\square$ Double Bend Achromat Lattice
$\square$ two super cells
$\square$ Circumference $L=48 \mathrm{~m}$.
$\square$ Nominal Energy $E=629 \mathrm{MeV}$.
$\square 8$ Bending Magnets $L_{B}=1.2 \mathrm{~m}$.
$\square$ Emittance
$\epsilon_{x}=120 \mathrm{nmrad}$.

## The Metrology Light Source

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## Fit parameters for the MLS

$\square 28$ horizontal BPM gains
$\square 28$ vertical BPM gains
$\square 12$ horizontal corrector magnets
$\square 16$ vertical corrector magnets
$\square 24$ quadrupole gradients
in total: $M=100$ fit parameters
Measuring data:
$\square 28 \times 12+28 \times 16$ data points included in the response matrix
$\square 28$ dispersion measurements
in total: $N=784$
number of the degrees of freedom $N-M=684$

$$
\chi^{2}=N-M \pm \sigma, \quad \sigma=\sqrt{2(N-M)}
$$

Predictor for the statistical error if $N-M$ is asymptotically large.

Fitting the focusing effect of the dipole

| Dipole model | $\frac{\Delta \text { Frac.Tune }}{\mathrm{kHz}}$ | $\frac{\chi^{2}}{D O F}$ | $\frac{\sigma(\text { mod. }- \text { mea.) }}{\mu m}$ |
| :--- | :---: | :---: | :---: |
| a) RBEND | $[28.6,233]$ | 307.5 | 5.32 |
| b) ditto, fit grad. | $[5.6,0.2]$ | 9.38 | 0.849 |
| c) $f_{\text {int }}=0.5$ | $[14.4,96.3]$ | 67.1 | 2.48 |
| d) ditto, fit $f_{\text {int }}$ | $[0.4,4.2]$ | 2.92 | 0.499 |
| e) ditto, fit grad. | $[2.0,3.4]$ | 2.45 | 0.459 |
| f) ditto, fit grad. <br> and fit $f_{\text {int }}$ | $[1.5,3.9]$ | 2.24 | 0.441 |

$\square$ Fitting fringe field or the gradient of the bending magnet dramatically improves the quality of the LOCO fit.

- Energy 629 MeV
- $\Delta$ Frac.Tune:

Deviation between measured fractional tune and the one predicted by LOCO
$\square$ length of the dipole 1.2 m

## Comparing LOCO's predictions with tune shift measurements



## The undulator U180

The undulator U180:
$\square$ Electro magnetic undulator with a period length of

$$
\lambda_{P}=180 \mathrm{~mm} .
$$

$\square$ causes considerable tune shift at lower energies.
$\square$ modeled as a sequence of dipole magnets.

Compensation schemes investigated:

| Energy | $\Delta \nu_{y}$ | Beta beat |  |
| :---: | :---: | :---: | :---: |
| MeV |  | $\max [\%]$ | RMS [\%] |
| 629 | 0.034 | 18 | 11 |
| 450 | 0.060 | 34 | 20 |
| 200 | 0.223 | 360 | 96 |

$\square$ opposite tune
$\square$ first tune then beta
$\square$ "alpha matching"
$\square$ tune bump

## Compensating the U180




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- Beam Energy is at 629 MeV

| mode | current | life time |
| :--- | :---: | :---: |
|  | mA | h |
| standard user mode | 135.0 | 13.9 |
| undulator on | 133.3 | 12.5 |
| opposite tune | 132.5 | 14.6 |
| first tune then beta | 131.5 | 12.6 |
| alpha matching | 130.6 | 14.0 |
| tune bump | 128.0 | 14.4 |

## Compensating the U180 at 200 MeV

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## Results

$\square$ Optics calibration works reliably both at the MLS and at BESSY II.

Fitting almost down to the noise level of the BPMs was achieved.
$\square$ Calibrated Model can be employed for realistic simulations.
$\square$ An orbit correction program including the focusing effects of IDs was build upon the model.
$\square$ Decoupling and symmetrizing the optics was successful at BESSY II.
$\square$ The focusing properties of IDs and the mitigation measures by the TFF were analyzed for the first time.

