Reason for direct wire readout for wirescanners ------

- 1. independent double check for maximum PMT readout at beam position => parallel using of PMT- and direct detected wire readout signals
- 2. replacement of PMT-readout

 - => omit the scintillator part
 => together with the PMTs and their HV-controlsystem at all

Two new ideas for direct wire readout for wirescanners

- 1. replace the classical charge preamplifier against a more noiseless one
- 2. use a "negative" convolution technique for data recognition

Charge Amplification with a logarithmic wide-bandwidth Peak Envelope Detector

- reference beam-charge : 5.5 * 10'6 electrons/bunch => 5.5 * 10'6 * 1.6 * 10'-19 C = 0.88pC => 1pC
- charge interaction space : ~ 1mm / space-dimension
- charge interaction time at the wire : ~ 3ps

- fundamental equation of system theory :

| Risetime of Inputsignal * Bandwidth of System = 0.35 | 0.35 ps * 1 THz = 0.35 | -> not realizable up to now

- necessity of input pulse stretching and charge amplification

- Q = C * U = I * t = U/R * t

- direct input of 8313 : 10 mVpp * 1 ns => Qin = 10 mVpp / 50 V/A * 1 ns = 1/5 pC

- leads to an output of 8313 : 50 mV \star 50 ns (Gaussian, treated as rectangle)

=> Qout = 50 mVpp / 50 V/A * 50 ns = 50 pC

- Charge amplification Qout/Qin : ~ 250 (if Rin = Rout)

List of problems to resolve

- sources for noise and their mathematical description
- equivalent network-model of the PED input network
- optimal filter theory for wire-signal-recognition
- other possible primary wire-detectors with preservation of phase-information of wire-signal
- insertion into the existing PMT readout chain
- parallel data-taking for PMT- and PED-signals

Signal recognition for the direct wire readout

- Moving Average Filter
- Wiener Filter
- Correlation: Matched Filter