# The CeB6 Electron Gun for the Soft-X-ray FEL Project at SPring-8

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SPring-8 / RIKEN Harima Institute

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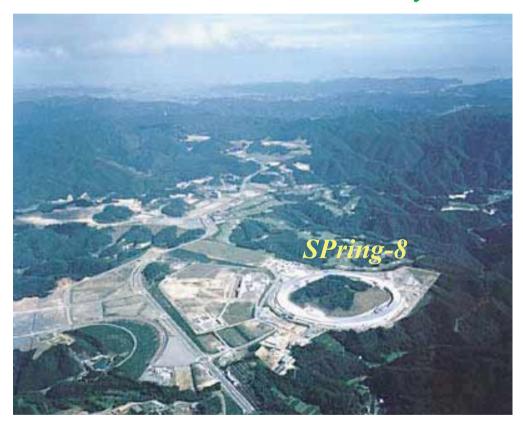
SPring-8 / RIKEN Harima Institute

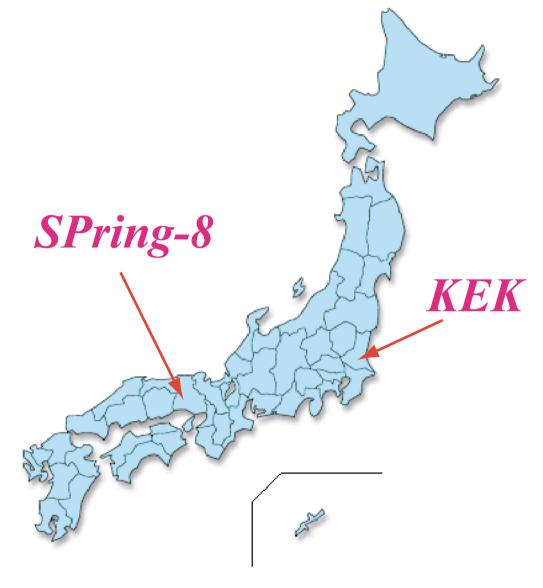
H. Matsumoto

High Energy Accelerator Research Organization (KEK)

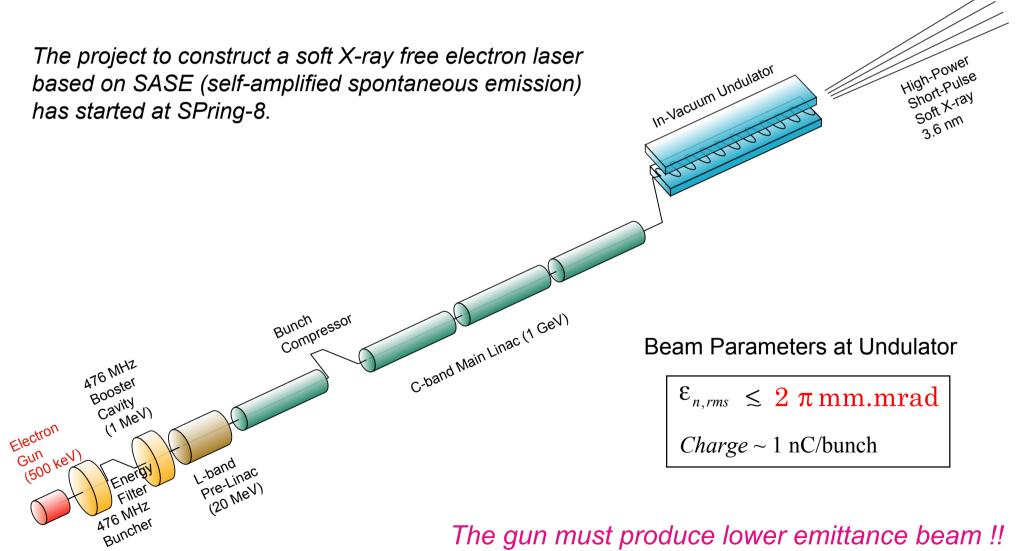
# Where is SPring-8?

Harima Science Garden City





# SPring-8 Compact SASE Source (SCSS Project)



The gun must produce lower emittance beam !!

# Requirements of X-FEL Electron Source

1) Low Emittance

 $<1 \pi$  mm.mrad

SASE-FEL Saturation

2) High Charge

~1 nC/bunch

3) High Beam Quality \_\_

No Beam Halo, No Dark Current

Precise Alignment
Protection of Undulator Magnet

4) Stable

Small Jitter, Long Lifetime

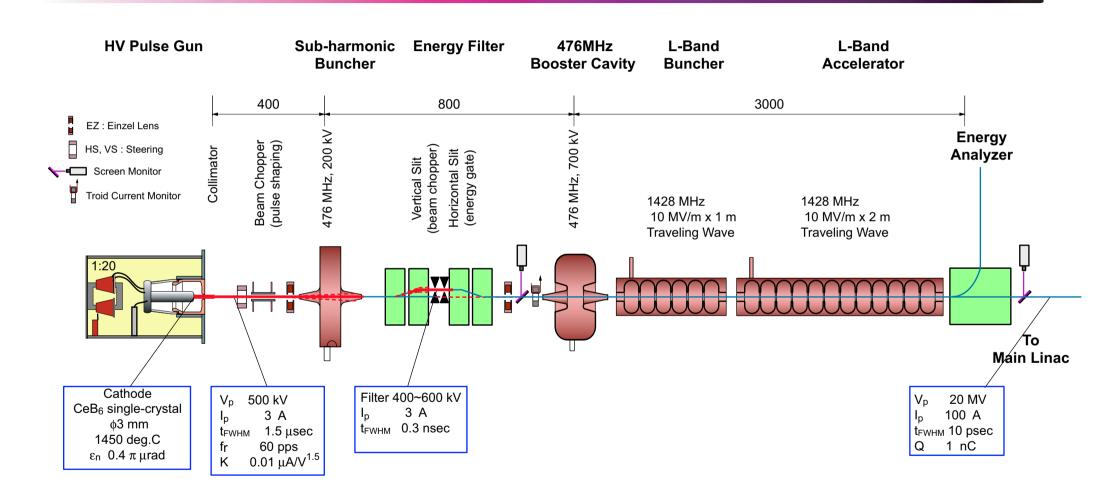
User Experiments

Thermionic Gun

RF-Gun

#### Low Emittance Injector for SASE-FEL

#### X-ray FEL



# Why do we use the HV thermionic gun?

# 1) Stable and Long Lifetime

- Simple.
- High power pulsed technology and thermionic cathode technology is well established, and used for various electron devices.

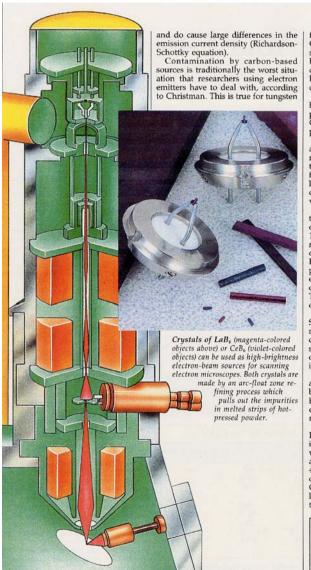
### 2) Low Emittance and Uniform Emission

- Single crystal cathode has very flat surface.
- Single crystal cathode provides uniform emission.

# CeB<sub>6</sub> Cathode Development

# CeB6 (Cerium Hexaboride) Single-Crystal Cathode

#### CeB6 cathode is widely used in electron microscope !!



filament, LaB<sub>e</sub>, and CeB<sub>e</sub> emitters. Carbon contamination hurts the emission properties of thermionic emitters by causing the work function to increase dramatically, thus resulting in higher operating temperatures and increased material volatility.

Severe contamination on hexaboride thermionic emitters can completely turn them off. However, the CeB<sub>6</sub> emitters can recover more completely than can LaB<sub>6</sub> emitters.

When carbon contamination, for example, gets on a filament, the operator must turn the power control higher to get emission back. This raises the filament temperature and shortens its lifetime. CeB's higher tolerance to contamination, therefore, is more relevant than the close work function.

To compare their respective contamination resistances, CeB<sub>6</sub> and LaB<sub>6</sub> crystals were exposed to acetone at 1670 K. Thermionic emission for both materials decreased to less than 20% of their original levels after exposure. However, increasing the emitter temperature to 1825 K and increasing the emission current returned the CeB<sub>6</sub> crystal to its original emission value. The LaB<sub>6</sub> crystal returned to only 24% of its original value.

When CeB<sub>6</sub> cathodes are heated in SEM environments, surface contaminants on the crystals are more quickly desorbed. The emission current also stabilizes more quickly than for LaB<sub>6</sub> once the cathode has reached operating temperatures.

Other rare earth hexaboride materials, including praseodymium hexaboride and samarium hexaboride, have been investigated as thermionic emitters, but this research has been minimal, says Christman.

CeB<sub>e</sub> cathodes can directly replace LaB<sub>e</sub> cathodes without any changes in instrument operating parameters and with no changes in brightness or total available beam current. About 35% to 40% of all electron-beam instruments currently use LaB<sub>e</sub>. For any of these, CeB<sub>e</sub> could more than double emitter life and improve contamination resistance.



#### **FEI Company**

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#### **Properties**

- Very flat surface (surface roughness <1 μm)</li>
- Low workfunction (~2.4 eV)
- Long lifetime (>10,000 hours)
- Rapid recovery from contamination

#### Design parameter of SCSS cathode

Thermal Emittance

$$\varepsilon_{n,rms} = \frac{r}{2} \sqrt{\frac{k_B T}{m_e c^2}} = 0.4 \, \pi \, \text{mm mrad}$$

Cathode Radius r=1.5 mmTemperature  $T=1450^{\circ}\text{C} (1723 \text{ K})$ 

Emission Current Density

Richardson-Dashman's Formula (Ideal Case)

$$J = 120.4 \ T^2 \exp(-\phi'/k_BT) > 42 \ A/cm^2$$

Boltzmann's Constant  $k_B = 8.617 \times 10^{-5} (eV/K)$ 

Effective Workfunction 
$$\phi' = \phi - \frac{e}{2} \sqrt{\frac{eE}{\pi \epsilon_0}} \sim 2.3 \ (eV)$$

# Property of CeB6 Cathode

#### Thermal Emittance

#### Normalized Emittance (RMS)

$$\varepsilon_{n,rms} = \frac{r_c}{2} \sqrt{\frac{k_B T}{m_e c^2}} = 0.4 \, \pi \, \text{mm.mrad}$$

Cathode Radius r=1.5 mmTemperature  $T=1450^{\circ}\text{C} (1723 \text{ } K)$ 



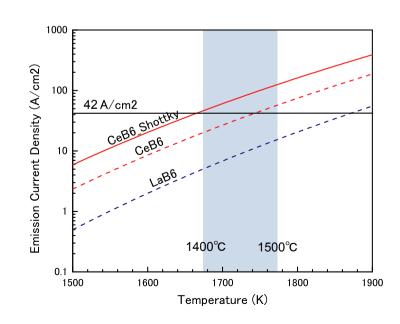
#### **Emission Current Density**

Richardson-Dashman's Formula (Ideal Case)

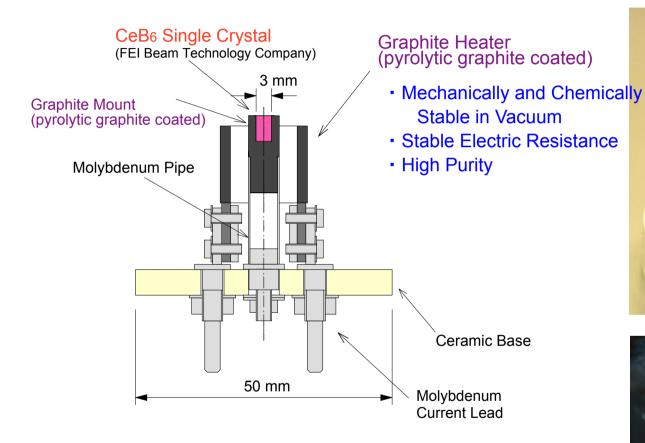
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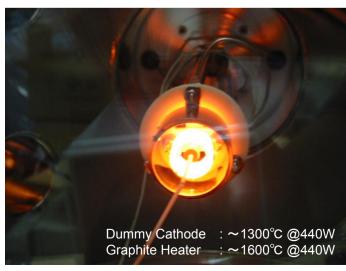
### CeB6 Cathode Assembly (First Model)



Operational Cathode Temperature ~ 1500°C (much higher than conventional cathodes)

Technical Challenge !!!





# Ceramic Base of Cathode Assembly



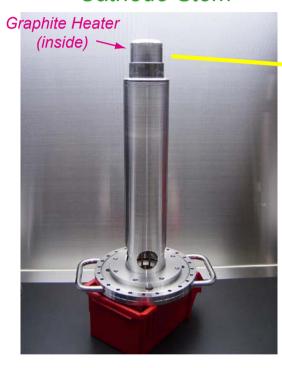
Alumina (Al<sub>2</sub>O<sub>3</sub>) ceramic base was broken by thermal heating.

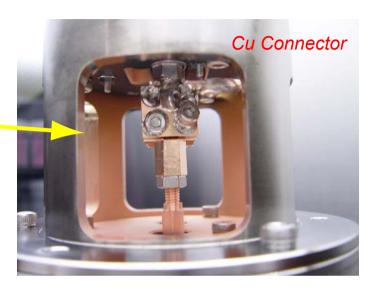
Si<sub>3</sub>N<sub>4</sub> ceramic base Very strong against thermal stress!!

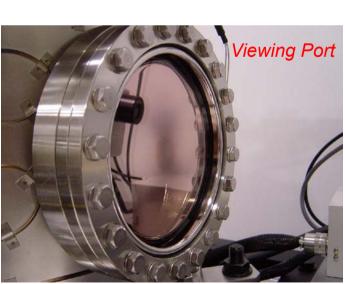


# Melting of Copper Connector

#### Cathode Stem





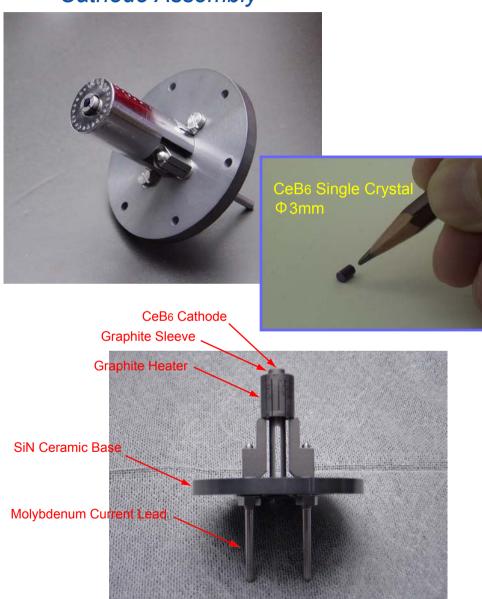




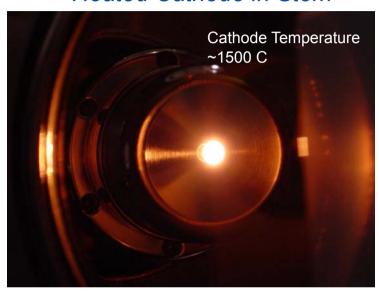


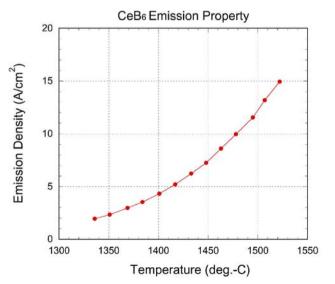
### CeB6 Cathode Assembly (New Model)

#### Cathode Assembly



#### Heated Cathode in Stem

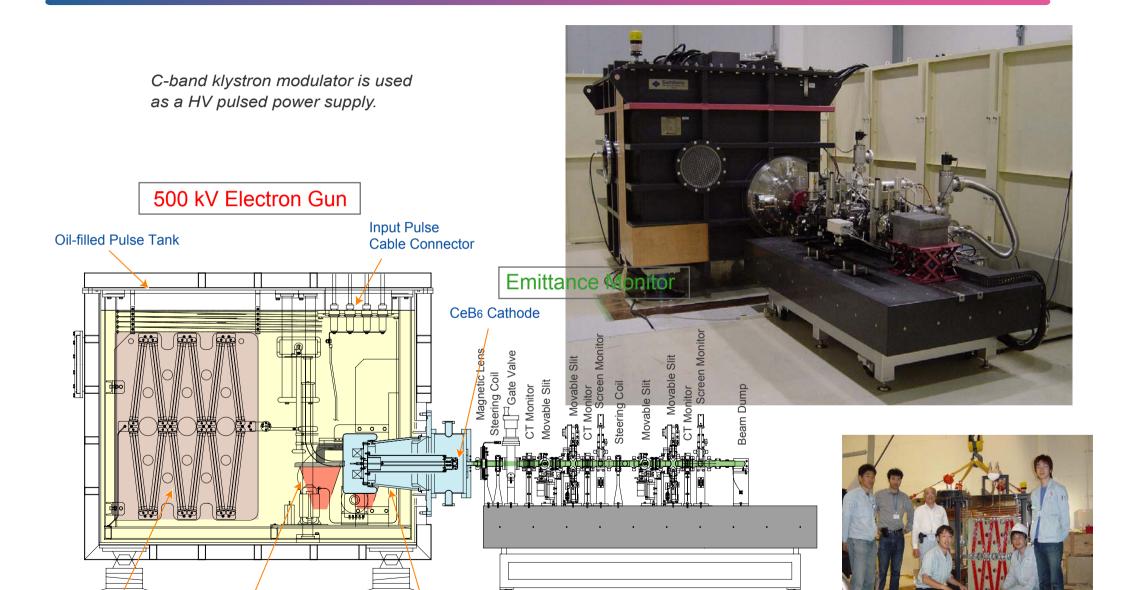




The gun voltage=500 kV Temperature was measured at the graphite sleeve by a radiation monitor.

# 500 kV Electron Gun

### 500 kV Electron Gun



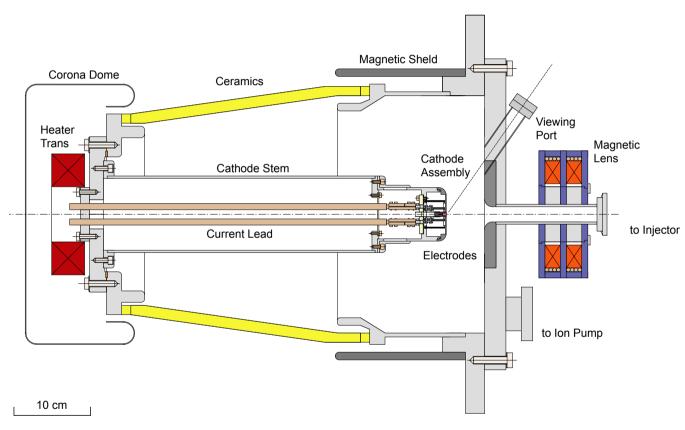
1 m

**HV Bushing** 

**Pulse Transformer** 

**Dummy Load** 

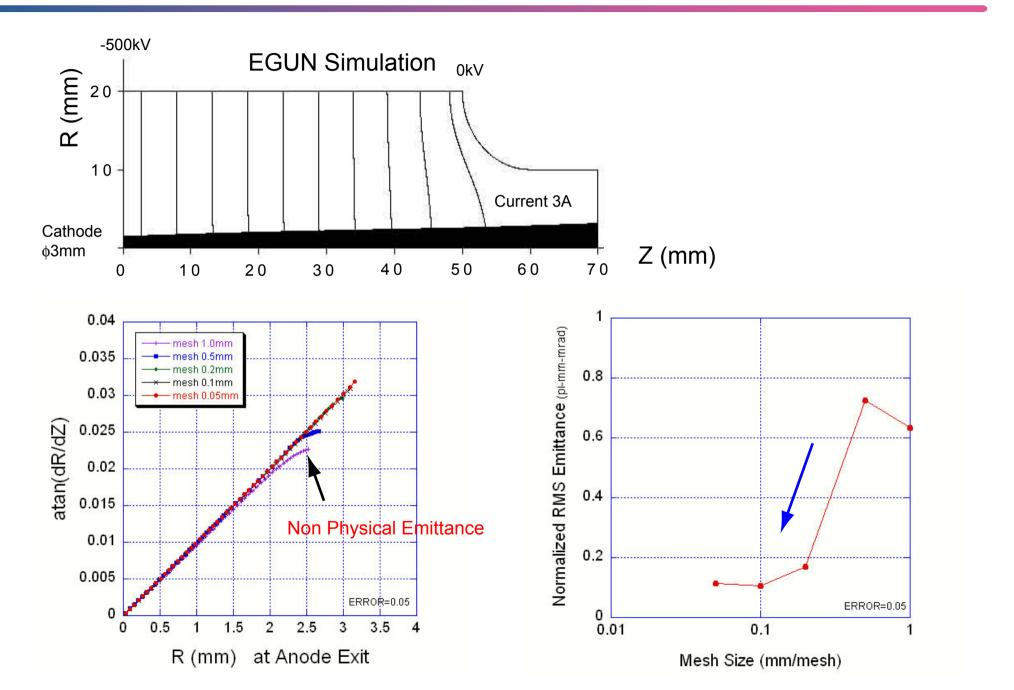
### 500 kV Electron Gun Chamber





Conceptual Design (2001)

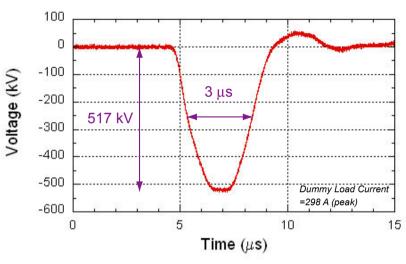
### Emittance at Gun Exit (Simulation)



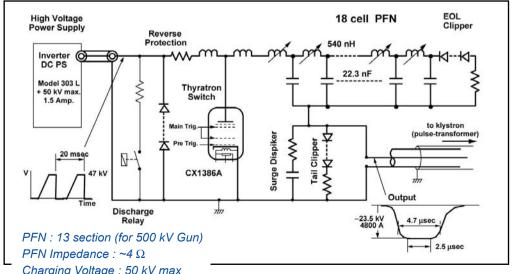
### C-band Klystron Modulator

Same model of the C-band klystron modulator is used for the 500 kV electron gun.

#### Gun Pulse Waveform



#### Circuit Diagram

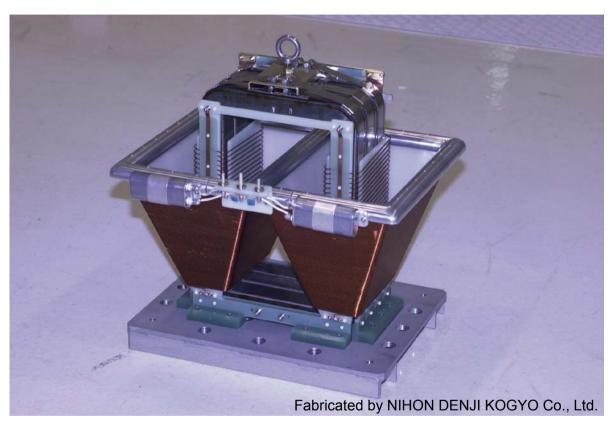


Charging Voltage: 50 kV max Max. Repetition Rate: 60 pps

# 500 kV Pulse Transformer

Conducted by Prof. Baba

#### Pulse Transformer of 500 kV Electron Gun



Turn Ratio

Input Pulse from Modulator

Output Pulse to Cathode& Dummy Load

Pulse Width

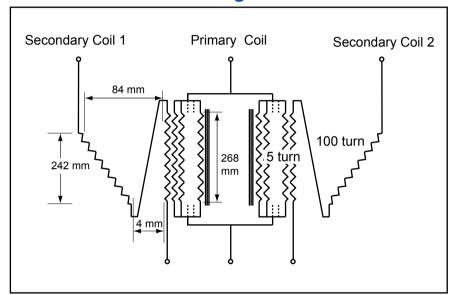
1:21

23.8 kV, 5502 A

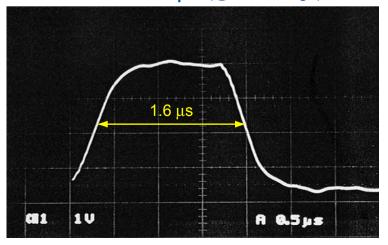
500 kV, 262 A

 $1.6 \mu s$ 

#### Winding Circuit



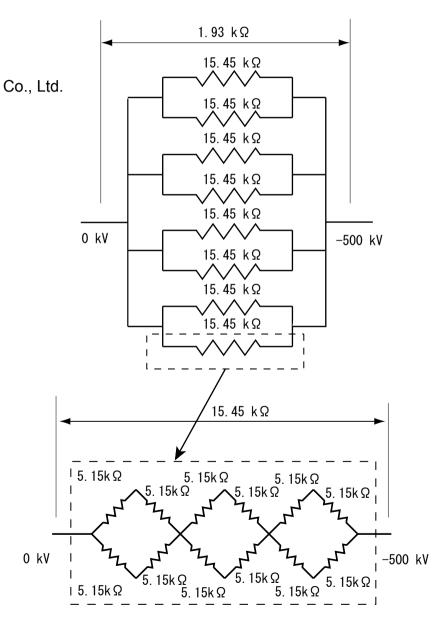
#### Pulse Shape (@Low Voltage)



# 500 kV Dummy Load



 $\begin{array}{lll} \bullet & \text{Pulse High Voltage} & 500 \text{ kV} \\ \bullet & \text{Peak Current} & 259 \text{ A} \\ \bullet & \text{Pulse Width} & 1.6 \text{ } \mu\text{s} \\ \bullet & \text{Dummy Load Impedance} & 1.93 \text{ } k \Omega \\ \bullet & \text{Average Power} & 12.4 \text{ } kW \end{array}$ 

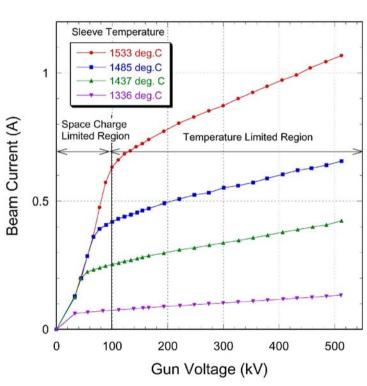


#### 500 keV Beam Production



#### Schottky Effect Droop of CT Monotor Space Charge Limit 0 Beam Current Gun Voltage (kV) Beam Current (A) -100 (CT Monitor) Beam Current (A) -200 0.5 -300 Gun Voltage -400 (CVD Monitor) -500 100 0 2 6 7 8 Time (µs)

#### **I-V** Curve



~1 ns part will cut out from the flattop by a beam deflector, and be used for the SCSS accelerator.

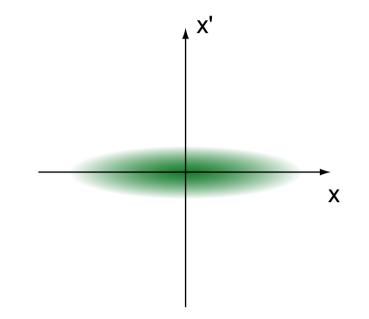
We operate the gun in temperature limited region to reduce emittance growth due to space charge.

# Emittance Measurement

### Normalized rms Emittance

#### **Definition**

$$\varepsilon_{n,rms} = \frac{1}{m_0 c} \sqrt{\langle x^2 \rangle \langle p_x^2 \rangle - \langle x \cdot p_x \rangle^2}$$
$$= \beta \gamma \sqrt{\langle x^2 \rangle \langle x'^2 \rangle - \langle x \cdot x' \rangle^2}$$



unit :  $\pi$  mm.mrad

$$\langle x^{2} \rangle = \frac{\iint x^{2}i(x, x')dxdx'}{\iint i(x, x')dxdx'}$$
$$\langle x'^{2} \rangle = \frac{\iint x'^{2}i(x, x')dxdx'}{\iint i(x, x')dxdx'}$$
$$\langle x \cdot x' \rangle = \frac{\iint x \cdot x'i(x, x')dxdx'}{\iint i(x, x')dxdx'}$$

$$r_c$$

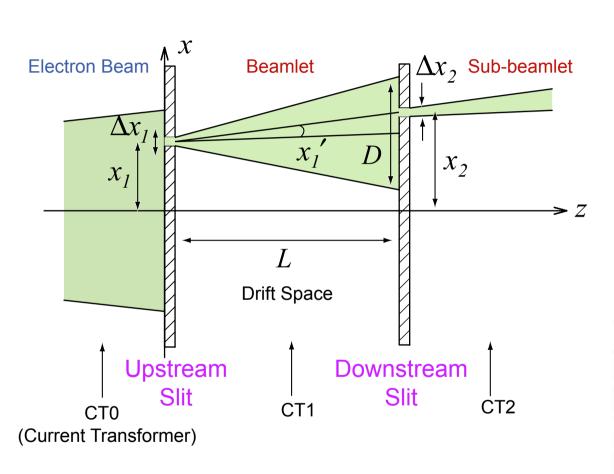
$$\varepsilon_{n,rms} = \frac{r_c}{2} \sqrt{\frac{k_B T}{m_0 c^2}}$$

 $=0.4 \pi$  mm.mrad

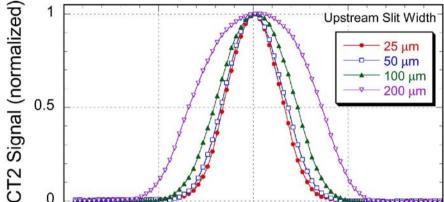
( 
$$r_c$$
 = 1.5 mm,  $T$  = 1723 K (1450°C))

0.5

### Emittance Measurement by Double-slits



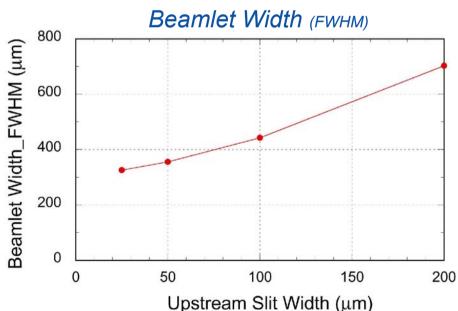
Beamlet spread due to space charge is about 15% at 50 µm width.



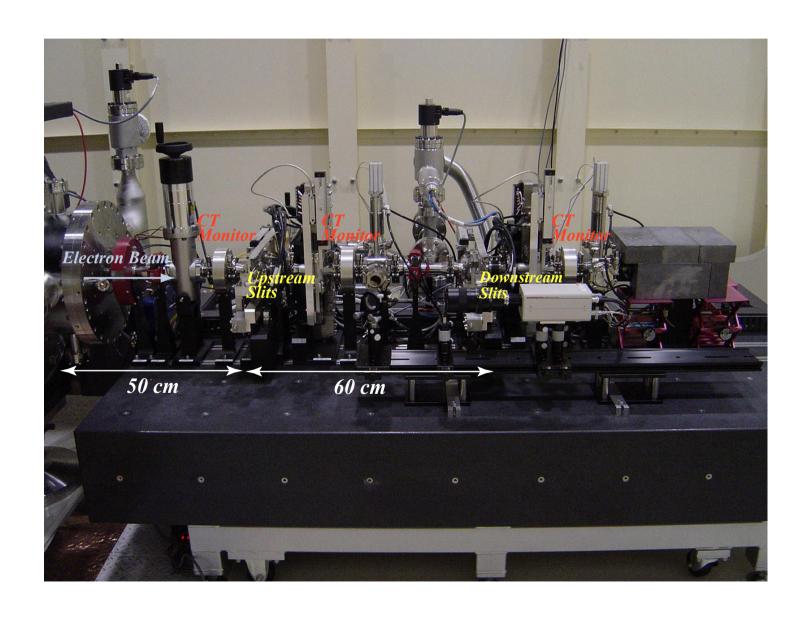
-0.5

Beamlet Profiles (400 keV, 0.9 A)

Downstream Slit Position (mm)

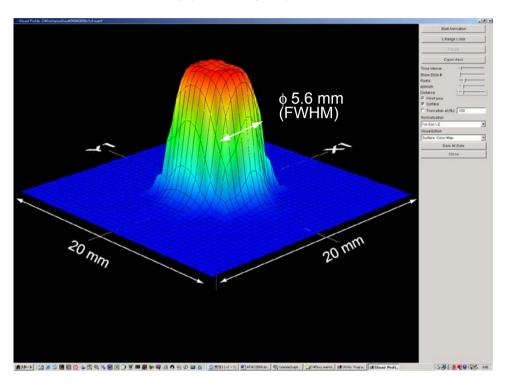


### **Emittance Monitor**

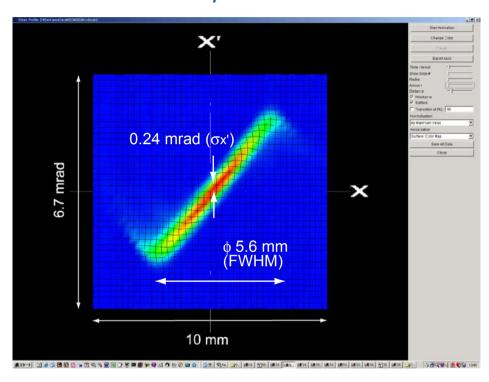


# Emittance of 500 keV Beam

#### Beam Profile



#### Phase Space Profile



Beam Energy : 500 keV Peak Current : 1.0 A

Pulse Width : 3 μs

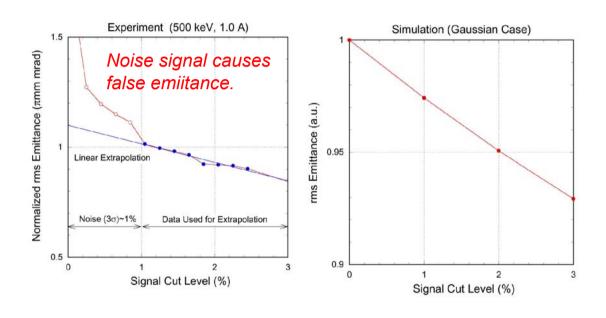
Emittance (En,rms)

Requirement : 2π mm.mrad @Undulator

Experiment :  $1.1\pi$  mm.mrad @Gun (preliminary)

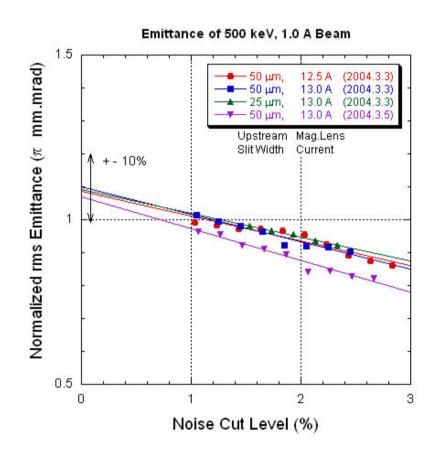
# Emittance Analysis

#### Analysing Method



- 1) Remove signal data whose amplitude is less than noise level ( $3\sigma$ ). Typically, the signal cut level is ~1% of the peak signal.
- 2) Data is corrected to zero cut level by extrapolation using linear function.

#### Reproduction



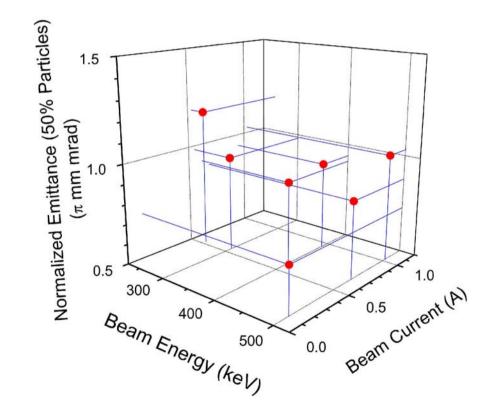
We need more studies about noise reduction and analysing method.

# Emittance Map

#### rms Emittance

#### 

#### Area Emittance including 50% particles



# Summary

1) We have succeeded in producing a 500 keV, 1 A beam from the CeB6 gun.

2) Measured emittance was  $\sim 1\pi$  mm mrad.

3) In 2004, we will construct a buncher system and measure the bunched beam emittance.